

Engineering Standard Track

CRN CS 250 TURNOUTS AND SPECIAL TRACKWORK

Version 1.3

Issued October, 2018

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Document control

Revision	Date of Approval	Summary of change
1.0	August, 2011	First Issue. Includes content from the following former RIC standards: TS 3103, TS 3104, TS 3105, TS 3202, TS 3501, TS 3502, TS 3504, TS 3509, TS 3645, RTS.3733, CTN 01/05
1.1	July, 2013	7.1.1.2 - Change to approval requirements for turnouts in vertical curves to reflect changes in CRN CS 210; Appendix 1 - Added definitions of switch types; Appendix 4 - Correction of value of 'e' for 1 in 15 crossing in Crossing Rate table
1.2	June, 2016	Various - Changed 'Principal Civil Engineer' to 'Principal Track and Civil Engineer'; Various - Rewording for consistency and minor corrections; Various - Correction of title errors; 5.2.1 - Add requirements for crossing geometry in diamond crossing; 7 - Added reference to Appendix 7; 7.1.3 - Added restriction on use of recovered turnouts with heeled switches in CWR track and requirement for recycled turnouts to be welded in CWR track; 7.1.6.1 Table 4 - Added note regarding adoption of HST speeds for appropriate rolling stock; 7.1.8 - New section "Security of points"; 11.2.1 - Reworded to clarify damage limits; Appendix 6 - Added statement regarding need to seek advice from PCTE before ordering certain products, Added space for and comment regarding Product Approval Numbers; Appendix 7 - New appendix - Approved special configurations (includes content of Waiver CCW 12/002) Various - Removal of requirement for diamonds, slips and expansion switches. These are not current CRN assets; 5.1.5 - Added requirement for turnouts in CWR to be welded; 6 - Minor inclusions to documentation requirements; 7.2.1 - Included note regarding use of timber throw off ramps; Appendix 7 - Updated to include content of Waiver CCW 15/018)
1.3	October, 2018	See summary of changes below

Summary of changes from previous version

Section	Summary of change			
Various	Removed requirements for swingnose and springwing crossings. These are not current CRN assets			
Various	Include consideration of derailer			
Various	Minor rewording throughout			
Various	Include consideration of the WPR2000 wheel profile for component design			
Various	Clarification that anchors are not permitted within the switch area			
2.2	Updated to include reference to signals standard CRN SD 014 - Points			
5	Include requirement to consider track drainage during design			
New 5.4.2	Added derailer requirement			
5.4.8	Clarify the "clear, even area" is the "clear, even throw off area"; Added additional commentary to explain that the throw off area is to minimise the risk of rolling stock roll over			
6.1	Inclusion of design report requirements			
6.2	Inclusion of design report requirements			
7.1.2	Table 2 – Removal of the Head Hardened rail from the alternative configuration & amended to make clearer preference for in-bearer on class 1 trackMinor amendment to wording to make clearer			

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7.1.3	Minor amendment to wording to make clearer that recovered turnout components shall not be installed on Class 1 track unless approved by the Principal Track & Civil Engineer and included requirement to not contain RCF or squat defects			
7.1.4	Inclusion of requirement for rail to be profiled for new turnout installations			
7.1.5.1	Rewording to make clearer as to when concrete bearers should be used			
New 7.1.6.3	Inclusion of Crossing Nose Longitudinal Profiles previously in CRN CM 222			
7.1.7.1	Inclusion of fabricated stockrail with GIJ as part of "front" if insulated joint is required within the area of the "front"			
7.2.1	Removal of reference to Legacy Design			
11.2.1	Table 12 – Amended formatting			
Appendix 5	Table 16 updated to include omitted 500m radius in-bearer with backdrive layout			
Appendix 8	Inclusion of new appendix detailing Crossing Nose Longitudinal Profiles previously in CRN CM 222			
Appendix 9	Inclusion of new appendix detailing determination of speed of runaway train for derailer determination			

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1 Scope and application

This Standard establishes functional and design requirements, approved configurations, acceptance standards, damage limits and repair standards for the following elements of track infrastructure:

- turnouts,
- catchpoints/derailers

Other special trackwork such as diamond crossings, slips and expansion switches are discussed but not in use on CRN infrastructure.

It includes switch and crossing components.

It also includes manual points lever operation, but does not cover points operation where the points are connected to the signalling system.

It is applicable to all Country Regional Network (CRN) main line and siding tracks.

The standard also contains definitions of standard terminology relevant to turnouts and special trackwork (See Appendix 1).

2 References

2.1 Australian and International Standards

Nil

2.2 CRN documents

CRN CS 200 - Track System

CRN CS 210 - Track Geometry & Stability

- CRN CS 215 Transit Space
- CRN CS 220 Rail and Rail Joints
- CRN CS 230 Sleepers and track support
- CRN CS 240 Ballast
- CRN CP 204 Product Approval

CRN CP 251 – Turnout Components

CRN RS 001 – Minimum Operating Standards for Rolling Stock

CRN SD 014 - Points

2.3 Other references

Nil

3 Engineering authority

Design and selection of infrastructure detailed in this standard for use on the CRN may only be undertaken by persons who have been granted appropriate Engineering Authority by the Principal Track and Civil Engineer.

4 Description

Turnouts allow rail tracks to converge or diverge. They are an assembly of rail components comprising:

- Switch and stockrail assemblies
- V Crossings
- Checkrail units
- Closure rails
- Bearers
- Plates, fasteners and rail joints
- Point operating equipment

(See Appendix 2 for turnout component descriptions)

Catch points and derail devices provide a level of protection against train collisions at the junctions of sidings and main running lines. Catch points or derail devices are provided when required to conform with JHR CRN Signalling Design Standards.

Catch points and derail devices may be interlocked with a signalling system or operate via a manual lever.

Catchpoints are an assembly of:

- Switch and stockrail assemblies
- Closure rails
- Throw off rails
- Bearers
- Ramp (or derail) blocks
- Plates, fasteners and rail joints
- Point operating equipment

5 Design requirements

This standard has been developed in consideration of the following criteria:

- speed in each leg of the points and crossing structure (e.g. on the through and diverging tracks in a turnout structure) including consideration of maximum superelevation (cant) deficiency;
- service loads (and dynamic response) including effects of impact loading at the points and crossing wheel transfer locations, track alignment, maintenance standards, and traffic task;
- component material types and maintenance requirements (e.g. fabricated versus cast crossings, material hardness and hardening processes);
- servicing requirements (e.g. lubrication and adjustment);
- component, layout geometry and assembly details include the following:
 - bearer dimensions, location and orientation;
 - rail fastening baseplate and chair dimensions, location and orientation;
 - track radius or alignment curvature;
 - crossing angle and wheel transfer area cross-sectional geometry;
 - switch geometry and cross-sectional geometry;

- detailed component geometry;
- ~ flangeways and wheel opening dimensions;
- ~ check rail length, location and effectiveness, profile and end flaring;
- wheelset geometry (i.e. wheel cross-sectional profile and wheelset back to back);
- requirements for movable components where applicable, including the geometric fit for construction and maintenance in all switch and crossing positions;
- need for trailable points in yard operations
- requirements for rails, bearers and fastenings

All turnout and special trackwork designs shall consider track drainage requirements

5.1 Turnouts

Turnout general arrangements and components shall meet the requirements of Section 7.1 of this standard. Designs for turnouts comprising compatible individual components shall comply with standard configurations unless otherwise approved by the Principal Track and Civil Engineer.

The following criteria shall be used in the design of points and crossing configurations:

5.1.1 Turnout geometry

- 1. Nominal gauge shall be 1435 mm:
- 2. All turnout components shall be designed so that the rail is vertical (i.e. zero cant). The 1:20 cant in open track shall be transitioned to zero cant over a minimum of 3 sleepers clear of the turnout bearers.

5.1.2 Rolling stock interface

- Turnout components shall meet the requirements of CRN Engineering Standard CRN CS 215 "Transit Space". This shall include clearances between crossovers where such moves are permitted by signalling.
- The nominal dimension from the gauge face of the running rail of a crossing to the working face of the check rail (i.e. check rail effectiveness) shall be 1391 mm with a flangeway width of 42mm and a check rail gap of 43mm.
- 3. The design switch rail toe / stockrail open throw dimension shall be ≥ 100mm or otherwise to suit signalling equipment, if installed.
- 4. Switch rail throat opening shall be 60mm ± 5mm.
- The check rail end opening shall be flared, and provide an opening ≥ 80mm (≥ 85mm if the checkrail is adjustable) to the gauge face of the running rail at the flared end. The flare angle shall be as shown in Figure 1.

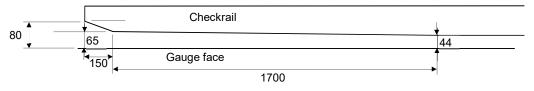


Figure 1 – Flare on checkrail end

- 6. Check rail height shall be between 0mm and 25mm above the running rail and shall take into consideration rolling stock clearances.
- 7. The design wheelset back to back dimension shall be 1357mm 1360mm as documented in CRN Engineering Standard CRN RS 001 "Minimum Operating Standards for Rolling Stock".

- 8. Flangeways shall be designed to accommodate a wheel flange height of \leq 45mm.
- The turnout components shall be designed to suit both ANZR 1 and WPR2000 new and worn wheel profiles.

5.1.3 Track geometry

- 1. The maximum superelevation (cant) deficiency allowable through the diverging track of a turnout shall be as detailed in CRN Engineering Standard CRN CS 210 "Track Geometry and Stability".
- 2. Design requirements for general track geometry including vertical/horizontal track alignment and superelevation are detailed in CRN CS 210.
- 3. Maximum design superelevation in turnouts shall be 50mm

5.1.4 Components

The design shall be based on relevant CRN Standards for the components used within the turnout.

5.1.5 Rail adjustment

Turnouts shall be designed as "fixed anchor points". Designs shall include suitable rail anchoring arrangements as specified in Section 7.1.12.

Turnouts located within continuously welded track (CWR) shall have rail joints welded out as detailed in CRN CS 220. V crossings due for renewal or replacement are an exception until replaced.

5.1.6 Signalling interfaces

Turnouts shall be designed to meet the signalling requirements specified by the Principal Signal Engineer. This includes requirements for

- the placement of insulated joints
- limiting conditions for the placement and operation of switch motors on power operated points, crossings, switches and drives, including limitations on the drilling of switches (hole size and location).
- in-bearer signalling
- conductive rails for signalling
- positive security of points that will be installed and over which rail traffic will operate before the signal interlocking is connected, or where the signal interlocking equipment will be removed from a set of points pending removal.
- Where non-standard carbon steels are proposed for use in switches or crossings a review of electrical properties shall be undertaken and signalling implications determined

5.2 Diamond crossings

Diamond crossings are not utilised in existing CRN infrastructure. They shall not be installed without the approval of the Principal Track and Civil Engineer.

5.3 Slips

Slips are not approved for standard application in CRN.

5.4 Catchpoints and derail devices

Catchpoint general arrangements and components shall meet the requirements of Section 7.2 of this standard. Designs for catchpoints comprising compatible individual components shall comply with standard configurations unless otherwise approved by the Principal Track and Civil Engineer.

The following criteria shall be used in the design of catchpoint configurations:

5.4.1 Catchpoint geometry

- 1. Nominal gauge shall be 1435 mm:
- 2. All catchpoint components shall be designed so that the rail is vertical (ie zero cant). The 1:20 cant in open track shall be transitioned to zero cant over a minimum of 3 sleepers clear of the bearers.

5.4.2 Derailers

- 1. Nominal gauge shall be 1435mm
- 2. All derailer locations shall be designed so that the rail is canted as per open track (1:20)
- 3. The application of derail devices are stipulated in CRN SD 014
- 4. Approach speed of a train to a derailer will be determined by the maximum of track speed in the siding/loop or speed of a train should a run-away occur. Guidance for runaway speed is provided in Appendix 9.

5.4.3 Rolling stock interface

- 1. Catchpoint components shall meet the requirements of CRN CS 215
- 2. The design switch rail toe / stockrail open throw dimension shall be ≥ 100mm or otherwise to suit signalling equipment, if installed.
- 3. Switch rail throat opening shall be 60mm ± 5mm.
- The design wheelset back to back dimension shall be 1357mm 1360mm as documented in CRN RS 001.
- 5. The turnout components shall be designed to suit both ANZR 1 and WPR2000 new and worn wheel profiles

5.4.4 Track geometry

Design requirements for general track geometry including vertical/horizontal track alignment and superelevation are detailed in CRN CS 210.

5.4.5 Components

- 1. The design shall be based on relevant CRN Standards for the components used within the catchpoint.
- 2. Catchpoints shall be of the same rail weight as the turnout they protect.

5.4.6 Rail adjustment

Catchpoints shall be designed as "fixed anchor points". Designs shall include suitable rail anchoring arrangements as specified in Section 7.2.2.

5.4.7 Signalling interfaces

Catchpoints shall be designed to meet the signalling requirements specified by the Principal Signal Engineer. This includes requirements for

- the need for catchpoints at a particular location
- the functional requirements for the catchpoints
- the placement of catchpoints to suit placement of signals
- the placement of insulated joints

- limiting conditions for the placement and operation of switch motors on power operated switches and drives, including limitations on the drilling of switches (hole size and location)
- in-bearer signalling
- conductive rails for signalling
- positive security of points that will be installed and over which rail traffic will operate before the signal interlocking is connected, or where the signal interlocking equipment will be removed from a set of points pending removal.

5.4.8 Clearances

- 1. Catch points and derail devices shall be located to provide a minimum of 450mm clearance between the side of a vehicle on the running line and the derailed vehicle at the clearance point.
- 2. Throw-off rails shall be located so as to ensure the wheels of the derailing vehicle travel a path that ensures that the vehicle does not foul the running line.
- 3. The throw off rail shall be either parallel to the running line or at such an angle to it that a derailed vehicle will be deflected away from the main line.
- 4. Derail blocks shall be located so that the derailed wheel tracking in the "four-foot" will mount the derail block before striking the rail.
- 5. The location of catch points, derailers or other similar devices shall be selected to ensure that a vehicle derailed at such a device has a clear, even throw-off area to minimise subsequent damage. Derailed vehicles must not be directed into a building or onto any structure, particularly overbridges, transmission line poles, earthworks or over any embankment or directly into any cutting or retaining wall..

The clear, even throw off area required is dependent on the potential size and speed of any vehicle or train to be derailed and the nature of any retarding equipment or infrastructure (such as a sand drag) and will have to be determined for each site.

The normal minimum requirement at locations where the normal operating speed of vehicles is ≤ 25 km/h shall be 2 vehicle lengths (40m) beyond the point of derailment (the end of the stockrail).

Approval of the Principal Track and Civil Engineer is required for strategies proposed at locations where trains operate at higher speeds or where alternative retardation devices are proposed.

The establishment of a clear landing area MUST include consideration of the train descent down the ballast shoulder to minimise the risk rolling stock roll over. A standard ballast shoulder creates a twist (tending to tip a train over) as well as a severe dip. (See Figure 3).

A square even descent can be achieved using ballast (Figure 2 and Figure 4).

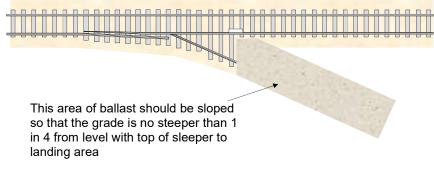


Figure 2 – Ramp to landing zone



Figure 3 – Example of catchpoint with poor landing zone



Figure 4 – Example of catchpoint with good landing zone

Special consideration must be given if there is any possibility of an occupied building being in the path of a derailed vehicle. This will include land outside the rail boundary where there is, or is the potential for, building development.

Bridge columns in the vicinity may need to be protected by deflection walls as specified in relevant Standards.

For locations where throw off and derail block configuration would not provide an adequate clear even run-off area, the following alternative arrangement is permitted.

- Retain the vehicle on the track from which it is derailed. In this case, the throw-off rail and derail block are not required.
- A detailed design is required on a case by case basis to provide an appropriate system to direct the derailed vehicle along the track. This can be achieved using a guard rail arrangement. The Principal Track and Civil Engineer shall approve designs
- 6. Catchpoints and derails at the ends of loops will normally be located in accordance with the guidelines specified in Table 1.

Track Centres	Catch point location		
Main line straigh	nt with parallel loop		
4 - 5m	Catch point or de-rail located on the parallel loop road with throw-off located at the tangent point		
6.4m	Catch point or de-rail located on the parallel loop road between the turnout and the loop road preferably on straight track		
Main line curved	I with concentric loop		
4 - 5m	Catch point or de-rail located on the concentric loop road with throw-off located at the compound tangent point		
6.4m	Catch point or de-rail located on the concentric loop road to provide specified minimum safety clearance as defined below.		

Table 1 - Catchpoint location at loop ends

7. Minimum safety clearances shall be met. These shall be calculated on the basis of track geometry and traffic type as follows:

$$C_{L} = W + 0.450 + \frac{B_{C}^{2}}{4R}$$

Where C_L = Safety Clearance (metres)

- W = Width of maximum vehicle operating in the track section (metres)
- B_C = Bogie Centres (metres)
- R = Radius of mainline or loop, whichever is less (metres).

The variables are defined in CRN CS 215

The distance from the throw off rail to the clearance point shall be $\frac{L-B_{C}}{2}$ metres i.e. equal to the distance from the end of the standard vehicle to the bogie centre (see Figure 5).

The standard distance from heel block to throw off rail is 1.625m,

The maximum design rolling stock gauges for vehicles are detailed in CRN CS 215:

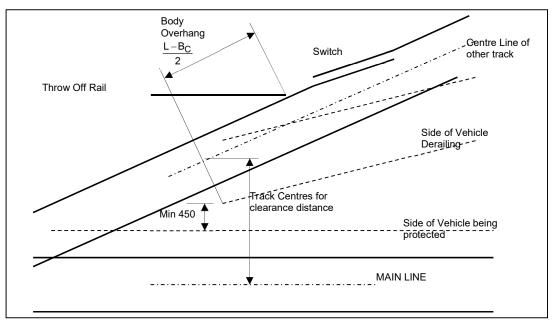


Figure 5 - Clearances at Catchpoints

5.5 Expansion switches

Expansion switches are not utilised in existing CRN infrastructure.

5.6 Manual points levers

Point lever general arrangements and components shall meet the requirements of Section 7.3 of this standard. Designs for point levers shall comply with standard configurations unless otherwise approved by the Principal Track and Civil Engineer.

The following criteria shall be used in the design of point lever configurations:

- 1. Manual point levers shall be designed to hold a closed switch against its matching stockrail with security, for safe vehicle movements.
- 2. Levers, or the points they control, may be locked or clipped to prevent unauthorised traffic movements.
- 3. Levers are operated manually and independently of an interlocked signalling system
- 4. Usage is restricted to shunting operations where traffic movements are directly controlled by operational personnel.
- 5. Manual point levers are not permitted on main lines.
- 6. Levers designed for trailable movements are permitted subject to operational requirements.
- 7. Manual point lever configurations shall be selected to meet the requirements of users.

6 Documentation requirements

6.1 Turnouts

Turnout designs shall include drawings detailing:

- turnout length
- switch length

- point arrangements including rail brace, slide chair and heel details and provisions for connecting rodding
- crossing and checkrail details
- rail weight
- bearer details
- plating details
- rail fastening and anchoring details
- setting out detail including curve radii, intersection points
- track grading through normal route and turnout road
- references to signalling designs as applicable

Detailed component manufacturing drawings shall be provided.

Designs relating to a specific layout shall include the following details:

- turnout framepoint co-ordinates
- location of points and crossing
- where there is no straight route in the turnout (i.e. the turnout is curved) offset dimensions shall be provided from a straight line
- crossing rate and catalogue No
- track centres
- track identification
- all proposed track alterations
- signalling requirements (supplied by signalling designer)
- location of insulated joints

Design reports are to be included in the works package and shall include

- Indicate areas of non-conformance to CRN standards
- Options assessed and reasons for abandoning the development of the option

6.2 Catchpoints and derailers

Catch point and derail designs shall include drawings detailing:

- point arrangements including rail brace, slide chair and heel details and provisions for connecting rodding
- throw-off rail details
- ramp (or derail) block details
- rail weight
- bearer details
- plating details
- rail fastening details
- setting out detail
- clearance points and signage if required

Detailed component manufacturing drawings shall be provided.

Designs relating to a specific layout shall include the following details:

- framepoint co-ordinates
- location of points and throw-off rail
- location of clearance point
- where the catchpoint is designed for installation in a curve, offset dimensions shall to be provided from a straight line
- details of clear area required beyond the point of derailment including identification and assessment of any obstruction or other hazards in the area
- track centres
- track identification
- all proposed track alterations
- signalling requirements (supplied by signalling designer)
- location of insulated joints

Design reports are to be included in the works package and shall include

- indicate areas of non-conformance to CRN standards

7 Options assessed and reasons for abandoning the development of the optionAllowable configurations

Note: Approved non-standard configurations are documented in Appendix 7.

7.1 Turnouts

Turnout configurations adopted for a specific site or application shall conform to the design requirements detailed in this standard unless otherwise approved by the Principal Track and Civil Engineer.

All new turnouts and replacement components shall be manufactured to meet the requirements of CRN Engineering Specification CRN CP 251 "Turnout Components".

There are two types of turnout used in the CRN:

- Conventional
- Tangential turnouts

The distinction between the two types is based on geometry and component technology.

Both conventional and tangential turnouts may be either

- standard, where one route is straight, or
- non-standard (or special) where the mainline route is curved

Conventional turnouts

Standard conventional turnouts are defined by a combination of the switch length and heel angle, and the crossing rate. (See Appendix 4 for a description of conventional turnouts). Conventional turnouts may be left or right hand.

Standard conventional turnouts are designed with the main line track straight.

There are three standard design options for conventional turnouts:-

- A fully straight crossing available for all turnouts with crossing angles ≥ 1 in 9. (See Appendix 4 Figure 8)
- A partially curved crossing (short leg curved to turnout radius long leg straight) available for turnouts with crossing angles ≤ 1 in 10.5 (See Appendix 4 - Figure 9)
- A fully curved crossing (short and long legs curved to turnout radius) available for turnouts with crossing angles ≤ 1 in 10.5.

Only approved designs shall be used within the CRN. The standard conventional turnout configurations for new installations are detailed in Appendix 4 - Table 13.

Tangential turnouts

Tangential turnouts are defined by the radius of the turnout. (See Appendix 5 for a description of a tangential turnout)

Tangential turnout designs have a standard configuration (footprint). The standard configurations adopted in CRN are detailed in Appendix 5 - Table 14.

All tangential turnout designs shall be based on an approved configuration. Each of these configurations has the through road straight and the turnout track, including the switches, continuously curved with a tangent point located near the toe of the points.

There are two standard configuration options for curvature through the crossing - either a straight crossing or fully curved crossing. (See Appendix 5 - Figure 10 and Figure 11).

Only approved designs shall be used. Suppliers shall submit designs to the Principal Track and Civil Engineer for type approval in accordance with Engineering Specification CRN CP 204 - Product Approval.

7.1.1 Location of turnouts

7.1.1.1 Horizontal alignment

Installation of turnouts in curves is NOT desirable. Where a new or replacement turnout is proposed in a horizontally curved section of the main line the following requirements apply:-

- 1. Configuration approval is required if any turnout (new or replacement) is proposed to be located on a curved section of track.
- Approval is required from the Principal Track and Civil Engineer to locate any turnout on curves <600 metres radius
- 3. Main lines shall be graded coplanar where track centres do not allow for turnouts forming the crossover to be treated separately.
- Turnouts should NOT, normally, be placed in transitions. If this cannot be avoided, the twist created through the switch and crossing segments of the turnout shall meet the normal twist limits for plain track geometry detailed in CRN CS 210.

7.1.1.2 Vertical alignment

Where a turnout is to be renewed or placed in a vertically curved section of the main line the following requirements apply:-

1. Track through turnouts and for 5m in front of switch tip shall be of constant gradient (no vertical curvature).

Configuration approval is required if the turnout (new or replacement) is not located on a constantly graded section of track.

Turnouts may only be constructed on vertical curves following a detailed assessment of maintenance impacts and risk.

2. If turnouts are approved on vertical curves, minimum radius (R_v) of the vertical curve for the length of the turnout plus 5 metres of track in front of the switch tip shall be as specified in CRN CS 210.

7.1.1.3 **Proximity to other special trackwork**

Special trackwork geometry shall be designed using standard units that can each be replaced as single units, with the exception that standard crossover designs shall make provision for use of long bearers crossing both tracks.

7.1.2 Selection of turnout type

Turnout type shall be selected to, at least, meet the minimum requirements specified in Table 2.

Tangential turnouts are the preferable configuration and may be used where conventional turnouts are specified as the minimum.

		New or replacement Turnouts						
	Frack Class	Turnout turno	Rail size		Bearer type		Switch	Crossing
		Turnout type	Pref	Alt	Preferred	Alternative	type	type
Main	line						·	
1	Preferred	Tangential	60		Concrete with in- bearer	Concrete, Steel, Timber	Tangential	Compound
	Alternative	Conventional	60	53	Steel	Timber	Flexible	Fabricated
2	Preferred	Tangential	60		Concrete	Steel, Timber	Tangential	Compound
	Alternative	Conventional	50	47, 53	Steel	Timber	Flexible	Fabricated
3, 5	Preferred	Conventional	50	47, 53	Steel	Timber	Flexible	Fabricated
Sidin	Siding (speed limited to 25km/h)							
1	Preferred	Conventional	60	53, 50	Steel	Timber	Flexible	Fabricated
2,3	Preferred	Conventional	50	47, 53	Steel	Timber	Flexible	Fabricated

Table 2 – Selection of Turnout type – Minimum requirements

- 1. Configuration approval is required if the turnout type detailed in Table 2 is not proposed for new or replacement turnouts.
- 2. Where a conventional turnout design is selected for a main line application, only standard conventional turnout designs shall be used. (See Appendix 4 Table 13).
- 3. Where the through track in main lines is installed on a curve <800m radius, and the turnout track is also curved. "Special" designs, which are non standard, are required for conventional turnouts. In such cases tangential turnout designs shall be used. (See Appendix 5 Table 14)</p>
- 4. Non standard conventional turnouts may only be installed in mainline track with the approval of the Principal Track and Civil Engineer. The design requirements for non standard tangential turnouts are detailed in Section 7.1.9
- 5. Configuration approval is required if non standard designs are proposed for siding applications.
- 6. Where an increase in turnout speed is desirable the use of tangential turnouts is recommended. A tangential turnout replacing a conventional turnout will normally allow a higher speed.
- 7. Where there is more than 2 MGT traffic on the turnout road the use of tangential turnouts is recommended

8. Conventional turnouts should generally be restricted to sidings and slow speed, low traffic, turnouts on the main line.

7.1.3 Use of recycled turnout material

Recovered material (either components or complete configurations) shall not be installed on Class 1 line, unless approved by the Principal Track & Civil Engineer.

Where recovered material is to be used, the components shall be assessed for compliance with the following requirements

- 1. Rail wear shall meet the classification limits given in Table 4 of CRN Engineering Standard CRN CS 220 "Rail and Rail Joints" for Category 1 (White Rail) or Category 2 (Blue Rail).
- 2. Rails shall be ultrasonically tested and visually inspected and have
 - No reportable defects (see Table 14 of CRN CS 220)
 - No visible web fillet cracks
 - ~ No head or foot cracks
 - No crush or laminated head
 - ~ No visible RCF or Squat defect
- 3. Wheel burns more than 3mm deep shall be removed or corrected
- 4. Visible end batter shall be removed or corrected if rail is to be classified for reuse in mainlines
- 5. Rail shall not have excessive rust
- The gauge face shall be re-profiled to the correct rail profile by removing any lip that has developed
- Gauge face angle shall not exceed 24° to the vertical when the worn face is within 15mm of the lower edge of the rail head

When replacing turnout components (switches, stockrails, crossings and checkrails) recycled components shall be of the same rail weight as the component they replace.

When replacing complete turnouts, recycled components shall, as a minimum, be the same rail weight as the turnout they replace.

Recovered turnouts with heeled switches shall not be installed in CWR track.

Recovered turnouts installed into CWR track shall be fully welded (i.e. no mechanical joints).

7.1.4 Rail

Rail used in the manufacture of turnouts shall meet the requirements of CRN CS 220

Rail size shall be selected for a turnout in accordance with the requirements of Table 2.

All new turnout installations shall be profiled to meet the requirements of CRN CS 220

7.1.5 Bearers

7.1.5.1 Selection of bearer type

Concrete, steel and timber bearers shall meet the requirements of CRN Engineering Standard CRN CS 230 "Sleepers and track support".

Concrete or timber bearers will, normally, be selected for a turnout in accordance with the requirements of Table 2.

Timber bearers shall only be used as an alternative to concrete or steel bearers (where specified in Table 2) at locations where it is impractical to design for concrete or steel. The alternative use shall be verified by the designer.

Notwithstanding the requirements detailed in Table 2, where concrete sleepers exist on the adjoining track, concrete bearers should be used.

Similarly, where steel sleepers are installed in the adjoining track, steel bearers should be used.

7.1.5.2 Bearer layout

The layout for turnout bearers or ties, as well as interface requirements for fixing components (crossings, checkrails, switch/stockrails and closure rails), shall be included in the design.

Turnout bearers in **conventional turnouts** are set out square to the main line alignment. This includes crossovers and any infill between turnouts

The turnout bearers in **tangential turnouts** are set out in a fan shape, with each bearer forming a half angle with both the main line and turnout road. This allows a single set of turnout bearers and plates for both a right hand and left hand turnout of similar radius.

The first sleeper installed beyond the bearers behind the crossing (mainline and turnout roads) shall be angled to return the sleeper skew to square to the track (angle $\frac{1}{2}$ difference between bearer skew and normal to the track).

For crossovers designed with tangential turnouts, the bearers are set out normal to the main lines. Long bearers shall be installed where clearance is not available for standard sleepers on adjoining tracks.

The bearer design for a nominated tangential turnout configuration is standard and can be used independently of the manufacturer of the steel componentry.

7.1.5.3 Use of In-bearers

The use of approved in-bearers (where the signalling equipment is contained within the bearer) is encouraged.

The layouts are only for use in tangential turnouts with concrete bearers. Standard concrete beams are used except for the bearers that are replaced by in-bearer units.

In the points area there is some respacing of bearers to suit the in-bearer A and B ties and the backdrive. The A and B in-bearer units are the same for all turnouts.

The back-drive units are of two types: Type 1 which suits 250m and 300m radius designs and Type 2 which suits 500m.

7.1.6 Crossings

7.1.6.1 Selection of crossing rate

The selection of the crossing rate shall be based on the geometric design of the turnout and the associated limiting speed of the turnout road.

Turnout speeds shall be determined by applying design standards for track geometry detailed in CRN CS 210.

Allowable published speeds for turnouts are as shown in Table 3. The speeds indicated are for normal passenger and freight trains.

Turnout Rate	Straight/ Curved	Switch length	Recommended Turnout Speed (km/h)			
Standard Convent	Standard Conventional					
1 in 8.25	Curved	6100 switch	15			
1 in 9	Straight	6100 switch	20			
1 in 10.5	Straight	6100 switch	25			
		9150 switch	40			
1 in 15	Straight	9150 switch	50			
Standard Tangenti	al	·				
Turnout radius: Crossing rate						
190:7	Curved		35			
190:9	Straight		35			
250:8.25	Curved		40			
250:10.5	Straight		40			
300:9	Curved		45			
300:12	Straight		45			
500:12	Curved		60			
500:15	Straight		60			
800:15	Curved		75			
800:18.5	Straight		75			
1200:18.5	Curved		85			
1200:24	Straight		85			

Table 3 – Turnout Speeds

- 1. Where there is a straight of 13m or longer between turnouts of a crossover, the speeds applicable to the individual turnouts shall be applied.
- The allowable speed through a crossover or reversing movement where the intervening straight section of track is < 13m shall be calculated on an individual site specific basis in accordance with the requirements of CRN CS 210.
- 3. Speeds for non-standard turnout designs shall be calculated from geometries in CRN CS 210 using Virtual transitions where required.

Crossings in main lines (other than swingnose crossings) introduce a design dip in the track. This is an impact point that leads to accelerated deterioration of components. The impact can be reduced by limiting the speed over the crossing. Whilst this is achieved for traffic travelling on the turnout road because of the crossing alignment geometry in Table 3 above, the speed of mainline (through road) traffic should be limited by the dip angle. As a guide the crossing angle should be selected to meet the design speed requirements in accordance with Table 4.

Crossing	Crossing	Mainline Speed over Turnout(kph)			
Rate (1 in)	Rate Angle		Maximum Note 1, Note 3	Exceptional	
2	140	16	25	29	
4.5	62	37	55	65	
7.5	37	62	92	108	
8.25	34	68	102	115	
9	31	74	111	1	
10.5	27	86	115	1	
12	23	99			
15	19	115	1		
18.5	15				
21	13	1			

Table 4 – Maximum mainline speeds for crossings based on dip angle

- Note 1. Maximum speeds shall only be introduced with the approval of the Civil Maintenance Engineer who must accept the increased maintenance impact.
 - 2. Exceptional speeds shall only be approved by the Principal Track and Civil Engineer.
 - 3. Equivalent HST speeds may be adopted for appropriate rolling stock with the approval of the Civil Maintenance Engineer who must accept the increased maintenance impact.

7.1.6.2 Selection of crossing type

The selection of crossing type shall be based on the requirements of Table 5.

Crossing type	Rail size		For use in turnout type
	New	Replacement	
Fabricated	50, 60	47, 50, 53, 60	Conventional
Rail Bound Manganese	60	53, 60	Conventional & Tangential
Compound	60	53, 60	Conventional & Tangential
Fully cast	60	60	Conventional & Tangential

Table 5 – Crossing types

- 1. Standard conventional turnouts can be provided with Fabricated or Compound "V" assemblies. See Appendix 2 for diagrams of each.
- Standard tangential turnout designs are approved for both straight and curved crossings. Where
 there are no site constraints or adverse impacts on other rail infrastructure the straight crossing
 type shall be used.
- 3. Standard tangential turnouts shall be provided with fixed nose compound crossings unless specified otherwise.
- 4.

7.1.6.3 Crossing Nose Longitudinal Profile

The selection of the crossing nose profile requires special attention, with different profiles to be applied depending on the design flangeway width, the wingrail profile and wheel profiles operating on the crossing.

CRN CS 250

The standard longitudinal profiles adopted by CRN are detailed in Appendix 8. The default profile adopted at manufacture is the T1 longitudinal profile, and would need to be adjusted to suit the installation location at during maintenance grinding. The correct longitudinal profile may be ordered from the supplier to reduce maintenance grinding requirement.

Alternate crossing nose profiles may be adopted in consultation with the Principal Track and Civil Engineer.

New crossings shall have punch marks installed on the wingrails at appropriate locations to allow identification of the theoretical point and other critical points required for crossing nose profile maintenance (ie 16mm and 32mm nose width locations).

7.1.7 Switches

7.1.7.1 Selection of switch type

Switch Type	F	Rail size	For use in	
	New Replacement of existing		turnout type	
Heeled	50, 60	47, 50, 53, 60	Conventional	
Flexible	50, 60	47, 50, 53, 60	Conventional	
Tangential	60	60	Tangential	

The selection of switch type shall be based on the requirements of Table 6.

Table 6 – Switch types

See Appendix 2 for diagrams of standard switch types

- 1. Switches for use with 47kg and 53kg rail have no machining on the stockrail and the switch rail is machined and vertically set to override the foot of the stockrail.
- 2. Switches for use with 50kg and 60kg rail have the stockrail undercut by machining to allow the switch to move partially under the head of the stockrail. The foot of both the switch and stockrail sit at the one level.

The undercut switch design eliminates the requirements for Heavy Duty and Housed Switches.

- 3. Switches for tangential turnouts are manufactured from a shallow depth asymmetric rail.
- 4. Where conventional turnouts are approved for use in main line applications, all new switches shall be the flexible type. There are however, limitations on the capacity of points operating equipment to operate flexible switches at remote distances. Where required by the Principal Signal Engineer, heeled switches may be used.
- 5. Switches used with Manual Levers (Thornley or Throwover) shall be, preferably, the flexible type
- 6. Switch protection pads shall be installed to protect conventional switches in siding turnouts where the crossing rate is ≤ 1 in 8.25. Apply the switch pad protector on one rail only 50mm in front of the appropriate switch (See Figure 6). Only approved bolt-on switch pad protectors may be used. Approved pad protectors are detailed in Appendix 6.

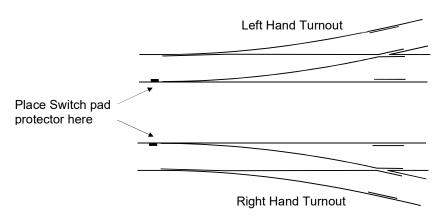


Figure 6 – Location of switch pad protectors

- 7. The operation of all new or renewed switches shall be determined by the Principal Signal Engineer. The switch operation shall be included in the turnout design.
- 8. The distance from the point of the switch to the nearest end of the stockrail is called the "front" of a turnout. The "front" is a standard length as shown in Table 7 and Appendix 2.

Switch Type		Rail size	Front length (mm)	For use in turnout type
Heeled		53	4877	Conventional
Flexible		53	4877	Conventional
Flexible	Flexible		2000	Conventional
Asymmetric	160 - 500	50, 60	2890	Tangential
	800		3490	
	1200		2290	

The front length shall normally be retained for all new turnouts and only altered in restricted location situations.

Table 7 – Front lengths of turnouts

Where an Insulated Joint is required within in the "front", the stockrail may be fabricated with Glued Insulated Joint included.

9. Where switches require renewal in an existing 53kg turnout, and there is no 53kg material available, the points may be renewed in 60kg material. Junction rails or welds shall be fitted between the switches and the crossing and associated check rails and appropriate plating shall be adopted.

Similarly, 47kg switch and stockrail units may be replaced by 50kg material.

7.1.8 Security of points

Where points will be installed and over which rail traffic will operate before the signal interlocking is connected, or where the signal interlocking equipment will be removed from a set of points pending removal, the points shall be secured against potential movement.

Traditionally with timber turnouts the points have been secured by spiking a fishplate to the timber bearer.

For bearers manufactured from concrete or steel, special spiking plates are required. The Principal Signals Engineer will review any proposal and confirm acceptance.

7.1.9 Design requirements for non-standard tangential turnouts

For turnouts in which both roads will be curved, the basic design shall be reconfigured to achieve the required geometry. In this case:

- the bearer design will be the same as for the standard turnout design but will need re-spacing to suit the altered track geometry
- the closure rails will be slightly shorter or longer depending on the extent of curvature applied in the design
- switch and stockrail design will be the same as for the standard turnout design but with altered curvature to suit the main line radius
- checkrail design will be the same as for the standard turnout design but with altered curvature to suit the main line radius
- crossings will need to be specially curved to suit the applicable geometry.
- Turnouts may be left or right handed.

7.1.10 Other special track components

In addition to the major components specified in this standard, all other special track components completing a standard turnout configuration such as fastenings, plating and closure rails shall be as specified on the General Arrangement drawings for each turnout type. Approval of a turnout design shall include approval of all special components included in the design.

7.1.11 Standard track components

Where standard plain track components are used in turnouts then the rail, rail joining methods, fastenings, sleepers/bearers, ballast, and track geometry used shall be designed in accordance with the relevant CRN standards detailed in Table 8.

Standard No	Component
CRN CS 210	Track Geometry & Stability
CRN CS 220	Rail and Rail Joints
CRN CS 230	Sleepers and track support
CRN CS 240	Ballast

7.1.12 Rail adjustment

The following rail anchoring requirements apply to turnouts constructed with timber sleepers and non-resilient fastenings. Bearers (timber, steel or concrete) with resilient fastenings do not require anchoring.

Only approved configurations shall be installed.

Double anchor every second sleeper for 32 sleepers (i.e. a total of 16 anchored sleepers) in front of the switch, commencing from the first sleeper from the switch.

Double anchor every second sleeper/timber for 32 sleepers/timbers (i.e. a total of 16 anchored sleepers/timbers) behind the crossing, commencing from the first timber after the crossing that has plain track fastenings.

Double anchor every second timber on the through rails and turnout rails between the heel of the switch and the front legs of the crossing.

Rail anchors are not to be installed in the switch area.

7.2 Catchpoints and derailer

7.2.1 General

Catch point or derail configurations adopted for a specific site or application shall conform to the design requirements detailed in Section 5.4 unless otherwise approved by the Principal Track and Civil Engineer.

All new catchpoints and replacement components shall be manufactured to meet the requirements of CRN CP 251

Table 9 details approved configurations for catchpoints used in main lines/crossing loops and in siding class tracks.

Track components comprising standard catchpoint configurations such as fastenings, plating and closure rails shall be as specified on the General Arrangement drawings for each catchpoint type.

Track Class	New or replacement catchpoints	
	Rail size (kg/m)	Drawing Reference
All	60	580 - 715
	53	153- 891
	47	300 - 696 ^(Note 1)

Table 9 - Approved catchpoint configurations

Note: 1 – Timber throw off ramps are to be replaced with mild steel design.

7.2.2 Rail adjustment

The following rail anchoring requirements apply to catchpoints constructed with timber sleepers and non-resilient fastenings. Catchpoints constructed with resilient fastenings do not require anchors.

Only approved configurations shall be installed.

Double anchor the catchpoint rail every second sleeper for 32 sleepers (i.e. a total of 16 anchored sleepers) in front of the switch, commencing from the first sleeper from the switch.

Double anchor the catchpoint rail every second sleeper/timber for 32 sleepers/timbers (i.e. a total of 16 anchored sleepers/timbers) behind the heel commencing from the first timber after the heel that has plain track fastenings.

Anchor the plain track rail as for plain track (see CRN CS 220).

Rail anchors are not to be installed in the switch area.

7.3 Manual points levers

Manual point lever configurations include:

- throw over levers
- sprung levers

Approved manual point levers, including proprietary designs, are detailed in Appendix 6.

8

Configuration requirements for existing special trackwork

Existing configurations of turnouts or catchpoints in each Track Class may not meet the requirements for new and replacement configurations (see Table 2 to Table 9). Speeds in Table 3 may not be achieved for these configurations.

All replacement components for existing turnouts shall be manufactured to meet the requirements of CRN CP 251

9 Undesirable configurations

The following configurations are considered undesirable for installation in main lines and should be considered for strategic upgrading.

- 1. Heeled switches
- 2. Short switches (< 5030m)
- 3. Turnouts on sharp curves, especially if they are similar flexure.
- 4. Special trackwork configurations such as diamonds, slips and expansion switches
- 5. "Entangled" trackwork, where different special trackwork units overlap.
- 6. Catchpoints without a clear landing area. Where such cases exist a risk analysis shall be undertaken to establish potential corrective or protective actions.

10 Acceptance standards for new installations

10.1 Turnouts

- 1. Turnout geometry for new installations shall meet the requirements of CRN CS 210. In addition:
 - gauge dimensions at the switch tip shall conform to the design ± 2mm.
 - ~ gauge at crossings shall conform to the design ± 2 mm
 - ~ flangeways at crossings shall conform to the design ± 1 mm
 - checkrail effectiveness shall conform to the design +3 –1mm
 - \sim switches shall bear on all plates + 1 0 mm in closed position
- 2. Other fabrication and installation tolerances shall be in accordance with the manufacturer's instructions.
- 3. When turnouts are placed within 30m of a bridge end (where spans are < 18m) OR when turnouts are placed within 60m of a bridge end (where one or more spans are \ge 18m but < 80m), the turnout shall be aluminothermic welded throughout and a flexible switch used if possible.
- 4. Where tangential turnouts are used, the turnouts, and the track for 50 metres either side, shall be fully welded. The use of joints is only permitted for a short period during the initial construction and installation phase. The Principal Track and Civil Engineer may, however, approve the installation of crossing units with fixed, swage fastened joints
- 5. For turnouts fitted with dry slide chairs, no oil or grease shall be applied to these chairs.
- 6. Plain track components shall meet the acceptance standards detailed in the component standards in Table 8.

10.2 Catchpoints

- Catchpoint geometry shall meet the requirements of CRN CS 210. In addition, gauge generally in catchpoints shall conform to the design ± 3 mm
- Other fabrication and installation tolerances shall be in accordance with the manufacturer's instructions.
- Plain track components shall meet the acceptance standards for component standards in Table
 8.

10.3 Manual point levers

Manual point levers shall be installed to meet the tolerances established by the manufacturer.

11 Repair standards

11.1 Geometry

11.1.1 Turnouts

The following maintenance limits shall be applied to manual regauging of turnouts or component renewal.

- 1. Turnouts shall meet the requirements of CRN CS 210
- 2. For non-interlocked points the clearance between the back of an open switch point and the gauge of the running stock rail shall conform to the design ± 2mm.
- 3. Housed switches shall conform to the design ± 1mm of the specified parameters.
- If the maintenance activity includes longitudinal movement of any crossing, the resulting position of the crossing intersection point (Theoretical Point) must be within 15mm of the position defined by reference pegs or survey monuments.
- 5. After maintenance, crossing and check rail measurements on all tracks shall be within the limits in Table 10.

	Flangeway Depth (min) (mm)	Crossing Flangeway Width (mm)	Checkrail Flangeway Width (mm)	Gauge (mm)	Checkrail Effectiveness (mm)
V Crossing	38 min	44 ± 2	44 ± 2	1435 ±2	1389 - <1396

Table 10 - Turnout geometry maintenance limits

11.1.2 Catchpoints

The following maintenance limits shall be applied to manual regauging or component renewal in catchpoints.

- 1. Geometry shall meet the requirements of CRN CS 210.
- 2. For non-interlocked points the clearance between the back of an open switch and the gauge face of the stock rail shall conform to the design ± 2mm.

11.2 Component repair

11.2.1 Switches

- 1. Repair of switches by wirefeed welding is prohibited. Switch profile and condition may only be repaired by grinding.
- 2. After maintenance switch tip measurements shall be within the limits in Table 11.

Parameter	Standard	Heavy duty	Undercut	Asymmetric
Switch tip radius	≥ 13mm	≥ 13mm	NA	NA
Switch angle (to vertical)	≤ 18° (to the vertical) (3:1)	≤ 18° (to the vertical) (3:1)	No part of the runni switch blade, betwe 30mm below the he form a plane at an 40° to the horizonta	en 17mm and ad of the rail, shall angle of less than
Switch tip height (below top of rail)	≥ 13mm	≥ 13mm	The top of the switch tip shall sit	
Switch tip width (at top of switch)	≤ 4mm	The whole of the switch tip shall sit within the gauge line of the joggled stockrail	within the face of th	e stockrail

Table 11 – Switch tip maintenance limits

3. There shall be no damage in the first 2m from the tip of the switch blade exceeding the criteria detailed in Table 12.

Switch tip damage		
Depth of damage below running surface of stockrail	Length of damage	
> 17mm	> 100mm	Single area of damage
	>100mm	Total length of multiple areas of damage less than 100mm apart
> 19mm	Any length	

Table 12 – Switch tip damage limits

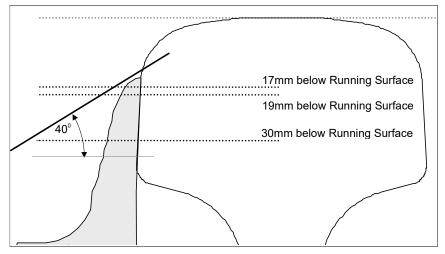


Figure 7 – Switch tip acceptance limits

11.2.2 Crossings and wingrails

- 1. Repair of crossings and wingrails by wirefeed welding is an approved repair method.
- 2. Repaired components shall meet the design profile and tolerances of the component being repaired.
- 3. All repairs shall be ultrasonically tested. ALL ultrasonic indicators must be below reportable limits as detailed in CRN CS 220.

Appendix 1 Definitions

Term	Description
Α	
Asymmetric Switch	Switches used with tangential turnouts. They are not machined from rail. They have a thick web and are shallower than conventional and undercut switches.
В	No Entries
С	
Catch points:	A single switch assembly and a throw-off rail. The catch point switch is normally set in the open position, thus breaking the continuity of the siding track causing unauthorised train movements to derail at a point clear of the main line.
Chair Plates	A chair is a flat plate with a pressed up section that is attached with a bolt through the web of either stockrail, in the case of a switch assembly, or the checkrail carrier, in the case of a checkrail assembly.
Check Rail	A rail placed inside the running rail which comes into contact with the back of the wheel flange and is used in points and crossing work to provide steering of the wheelset such that the crossing nose is not contacted by the opposite wheel
Checkrail Unit	The unit consists of a length of rail (called the checkrail) with a flared bevel machined on each end, hardened on the checking face, bolted through chocks to a closure rail (called the carrier) to attain a flangeway clearance.
	The centre of the checkrail is usually opposite the theoretical point of the crossing
Chocks	An iron casting used mainly with check rails and crossings to support rail components at a fixed distance apart. Raised lettering and numbers on the chock identify its application
Clearance Point	A point on converging or diverging tracks where the track centres or separation between the tracks allows clear passage for passing trains and beyond which vehicles must not stand.
Closure Rails	Rails making up a turnout apart from those in the points, crossings and checkrail units
Compound Crossing	Comprises a crossing V point that is manufactured from a single cast nose which is welded to head hardened rails to complete the V which replaces the point/housed rails in a fabricated crossing. They may be manufactured from manganese steel, chrome vanadium alloys or other materials
Compound Manganese Crossing	Is a Compound crossing V point that is manufactured from a cast manganese nose which is explosively hardened and flashbutt welded to head hardened rails to complete the V which replaces the point/housed rails in a fabricated crossing.
Conventional Switch	Conventional switches are machined from rails and tapered down from a full rail at the heel, to a thin point that fits closely against the stock rail. They are only in use with 53kg and lighter rail and are not used when turnouts are renewed.
Crossing Assembly	The component of a track system where lines branch out or intersect. Crossings assist in the passage of track wheels where two track rails intersect. Crossings may be fixed or switchable. In diamond crossings there are K and V crossings and in turnouts V crossings.
Crossover	The means by which trains pass from one track to an adjacent parallel track. A Crossover is constructed from two turnouts (one on each track facing opposite directions) and connecting plain trackwork
D	
Derail	A vehicle derailing device that, when operating to protect the main running line, causes wheels to climb the siding rail and derail clear of the protected line.
Diamond Crossing	The component of a track system where lines intersect. Diamond Crossings comprise V and K crossings.

Term	Description
E	
Expansion switch	An assembly comprising two rails appropriately matched and fastened at the longitudinal interface to provide virtual continuity of the running rail and gauge faces while allowing controlled longitudinal slip. Expansion switches provide a level of control for rail stresses when tracks are
	attached to sub-structures (eg steel underbridges) which are also subject to temperature related expansion and contraction.
F	
Fabricated Crossing	Comprises a Vee and two (2) wing rails fabricated from sections of rail, set, machined and fitted together with chocks. The hand of the crossing is determined by the location of the point rail and may be right or left. The point rail is always the rail carrying the maximum tonnages, or higher speed. A right hand crossing has the point rail in the rail that connects to the right hand switch.
Fixed crossings.	These crossings have a wheel flange gap in both rails. Wheel transfer of fixed crossings depend on matching wheel and rail profiles. Fixed crossings are used in conjunction with check (guide) rails to provide lateral guidance in the crossing area.
Flangeway	The space adjacent to the gauge face of a running rail to allow for the passage of wheel flanges.
Flangeway Clearance	The distance between the gauge side of a running rail and the guard face of a check rail or the guard face of a wing rail
Flangeway Depth	Flange way depth is the height of the running surface of the rail above the top of the blocks at check rails and in 'V' and 'K' crossings
Flare	The tapered widening at the ends of flangeways to gradually engage wheel flanges and position them to pass through flangeways.
Flexible Switch	A switch machined from longer rails and fixed towards the end of this rail with blocks or other device to the adjacent stockrail. The switch movement is provided by the flexibility of the longer switch rail and a section machined from the rail foot (foot relief) towards the fixed end.
Fully cast crossing	A one piece solid cast steel crossing with the four legs joined to standard rail sections through a welding process or by bolts and plates.
G	No Entries
Н	
Heavy duty switch	Switch with thickened switch points used in conventional turnouts with heavy traffic to limit wear. Used with joggled stockrails to ensure the running face of the running rail is colinear
Heel	The end of a switch at which the switch pivots
Heel Block	Single or multiple blocks, depending on switch type, that rigidly fix the switch rail to the adjacent rail in the correct geometric configuration. The adjacent rail is the stockrail and can include a closure rail for some switch types.
Heeled Switch	A switch that pivots about a gapped joint between the switch rail and adjoining closure rail. The switch is bolted to the stockrail and closure rail using a heel block and fishplate designed to allow this movement.
Housed Switch	A housed switch is a heavy duty switch and joggled stockrail equipped with a "Housing". The housing is a specially machined component with a hardened checking face fitting above the switch to act as a checkrail for the opposite switch and joggle. Where both switches are required to be heavy duty a housing is required on one of the switches.

Term	Description
I	
In - Bearer	A bearer fabricated into a hollow channel shape that is used at a set of points to house the switch operating rodding. This eliminates the rodding being located in a bay between bearers.
Interlocking	Interaction of equipment controlling switches and/or signals to prevent conflicting movements, and to make sure that routes are set correctly.
J	No Entries
К	
K Crossing	The principal special component of a diamond crossing. It is the intersecting component between two rails. The intersection creates an unchecked area in the centre of the K, thus limiting the angles that can be designed for K crossings
L	No Entries
М	
Manual Point Lever	An apparatus consisting of a manually actuated lever and connecting rodding to operate points in turnouts and catchpoints or to operate a derail device. Manual point levers do not include ground frame or signal box levers that are generally connected to an interlocked signalling system.
Ν, Ο	No Entries
Ρ	
Points and crossings	A combination of rail and track components that provide for one track to join or cross another whilst maintaining continuous support and direction to the rolling stock wheels. The points are the location where one track separates into two tracks (or vice-versa) and generally includes moving rail components called switches or switch blades. The crossing allows rolling stock wheels to cross over a rail. Combinations of points and crossings may be used to construct various track structures including slips, diamond crossings, turnouts and Catchpoints.
Points Assembly	The location where one track separates into two tracks (or vice-versa) and generally includes moving rail components called switches or switch blades that are attached to stockrails.
Q	No Entries
R	
Rail Brace	Component used in points assemblies to fasten the stockrail in position where fastenings on the gauge side of the rail cannot be used. The Rail Brace is bolted through the web of the stockrail.
Rail Brace Plates	Attach the Rail Brace to the bearer.
Rail Bound Manganese Crossings	Crossings with the actual crossing area made from manganese steel casting and surrounded by specially machined and set rail wings.
S	
Single/Double Slip	A special track layout that combines turnouts and diamond crossings. They allow train movements both across and onto and out of a track.
Spring Wing crossing	A switchable V crossing with both a fixed and spring wing leg. The spring wing effectively eliminates the flange way gap when using the main line thus reducing the wheel generated impact in the crossing. The wheel flange forces the spring wing open when taking the siding road
Stockrails	These provide support for the closed switch and become the running rail when the switch is open. They are curved, set and /or joggled.

Term	Description
Swing Nose Crossing	A switchable V crossing with a nose assembly that moves from the main line rail to the turnout rail, depending on the train movement, allowing a continuous surface for the wheel to run through the crossing. They are provided with straight crossings only. No check rails are required with this crossing type.
Switch	Is a machined tapered rail that allows the direction of a train to be altered to another line. A switch consists of a section of rail set and machined to a design shape, drilled to detail to accommodate switch operating rodding and heel blocks or chocks to allow attachment to a stockrail.
Switch Rollers	Rollers that support the switch during the opening and closing operation. The can be located in the bay between bearers, usually bolted to the stockrail, or be fabricated as a part of the plate assembly under the switch. They eliminate the need to lubricate the switch plate/switch interface.
Switch Stops	Switch Stops are bolted to the web of the stockrail and make contact with the web of the switch when the switch is in the closed position, providing lateral support. They can be manufactured from castings, rolled angle section or extended bolts.
Switchable crossings.	These crossings close the gap in one track that is being made active for traffic allowing a continuous surface for the wheel to run through the crossing. Wheel transfer in switchable crossings is without any impact for any wheel profile. Switchable crossings have no flange gap in the active track and thus do not require check rails. They can have either Swing Nose or Spring Wing
т	
Tangential Switch	A switch with a continuous curve through the full length of the switch. The curved gauge line of the switch is tangent to the gauge line of the attached stockrail at a distance in front of the switch tip
Theoretical Point	Located on the crossing nose at the intersection of the gauge lines of the two running rails forming the crossing
Trailable Point Lever	A manual point lever that is designed to allow for vehicle wheels trailing through points set the wrong way to re-set the points for the trailing movement without the need to operate the lever.
Turnout	Special trackwork that allows trains to pass from one track on a diverging path. It consists of switch and stockrail assemblies, a 'V' crossing and checkrails, linked together by straight and curved infill rails (closure rails).
Turnout Radius	The radius of the centreline of the curved turnout track and not the turnout rail radius. It is tangential to the switch at the heel (real or imaginary) and to the appropriate leg of a straight crossing. The radius is carried through a curved crossing
Turnout Rail	This is the closure rail that joins the turnout switch to the crossing, as part of the secondary track. It may consist of more than one rail length.
Turnout Length	The distance from the toe of the switch to the theoretical point measured along the main line running rail containing the crossing.
U	
Undercut Switch	Switches for use with 50kg and 60kg rail have the stockrail undercut by machining to allow the switch to move partially under the head of the stockrail.

Term	Description
V	
V crossing	A unit that allows a train travelling on the turnout direction rail to cross the mainline rail.
	The crossing rate is a measure of the angle made by the main line and turnout rail gauge faces that intersect at the theoretical point. The crossing rate is the cotangent of the angle made.
	All crossings are identified by markings on the wing rail which are provided during manufacture. See Appendix 2 Crossing Identification
	The catalogue number allows the geometry of the particular crossing to be identified. Each catalogue number defines a crossing with a unique geometry.
	See Appendix 2 for diagrams of standard crossing types
W	
Wing Rail	The rails of a crossing (on the end closest to the switch in a turnout) that are flared to allow the passage of the wheel to transfer to or from the crossing nose. Named for their resemblance to a wing in shape.
X, Y, Z	No entries

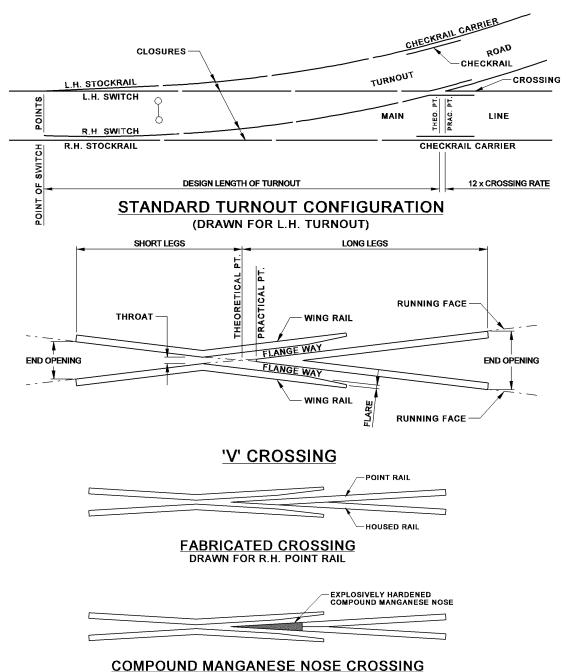
Grouped by component		
Term	Description	
General		
Points and crossings	A combination of rail and track components that provide for one track to join or cross another whilst maintaining continuous support and direction to the rolling stock wheels. The points are the location where one track separates into two tracks (or vice-versa) and generally includes moving rail components called switches or switch blades. The crossing allows rolling stock wheels to cross over a rail. Combinations of points and crossings may be used to construct various track structures including slips, diamond crossings, turnouts and Catchpoints.	
Turnout	Special trackwork that allows trains to pass from one track on a diverging path. It consists of switch and stockrail assemblies, a 'V' crossing and checkrails, linked together by straight and curved infill rails (closure rails).	
Turnout Length	The distance from the toe of the switch to the theoretical point measured along the main line running rail containing the crossing.	
Turnout Radius	The radius of the centreline of the curved turnout track and not the turnout rail radius. It is tangential to the switch at the heel (real or imaginary) and to the appropriate leg of a straight crossing. The radius is carried through a curved crossing	
Turnout Rail	This is a closure rail that joins the turnout switch to the crossing, as part of the secondary track. It may consist of more than one rail length.	
Stockrails	Provide support for the closed switch and become the running rail when the switch is open. They are curved, set and /or joggled.	
Crossover	The means by which trains pass from one track to an adjacent parallel track. A Crossover is constructed from two turnouts (one on each track facing opposite directions) and connecting plain trackwork.	
Diamond Crossing	The component of a track system where lines intersect. Diamond Crossings comprise V and K crossings.	
Catchpoints:	A single switch assembly and a throw-off rail. The Catchpoint switch is normally set in the open position, thus breaking the continuity of the siding track causing unauthorised train movements to derail at a point clear of the main line.	

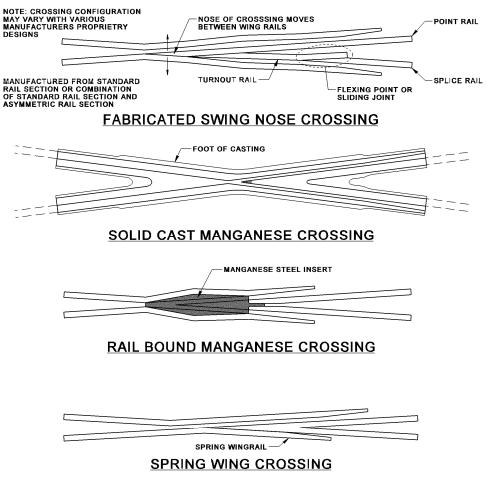
Term	Description
Clearance Point	A point on converging or diverging tracks where the track centres or separation between the tracks allows clear passage for passing trains and beyond which vehicles must not stand.
Derail	A vehicle derailing device that, when operating to protect the main running line, causes wheels to climb the siding rail and derail clear of the protected line.
Expansion switch	An assembly comprising two rails appropriately matched and fastened at the longitudinal interface to provide virtual continuity of the running rail and gauge faces while allowing controlled longitudinal slip.
	Expansion switches provide a level of control for rail stresses when tracks are attached to sub-structures (eg steel underbridges) which are also subject to temperature related expansion and contraction.
Single/Double Slip	A special track layout that combines turnouts and diamond crossings. They allow train movements both across and onto and out of a track.
Points	
Points Assembly	The location where one track separates into two tracks (or vice-versa) and generally includes moving rail components called switches or switch blades that are attached to stockrails.
Switch	A machined tapered rail that allows the direction of a train to be altered to another line. A switch consists of a section of rail set and machined to a design shape, drilled to detail to accommodate switch operating rodding and heel blocks or chocks to allow attachment to a stockrail.
Heeled Switch	A switch that pivots about a gapped joint between the switch rail and adjoining closure rail. The switch is bolted to the stockrail and closure rail using a heel block and fishplate designed to allow this movement.
Heel	The end of a switch at which the switch pivots
Heel Block	Single or multiple blocks, depending on switch type, that rigidly fix the switch rail to the adjacent rail in the correct geometric configuration. The adjacent rail is the stockrail and can include a closure rail for some switch types.
Flexible Switch	A switch machined from longer rails and fixed towards the end of this rail with blocks or other device to the adjacent stockrail. The switch movement is provided by the flexibility of the longer switch rail and a section machined from the rail foot (foot relief) towards the fixed end.
Tangential Switch	A switch with a continuous curve through the full length of the switch. The curved gauge line of the switch is tangent to the gauge line of the attached stockrail at a distance in front of the switch tip.
Conventional Switch	Conventional switches are machined from rails and tapered down from a full rail at the heel, to a thin point that fits closely against the stock rail. They are only in use with 53kg and lighter rail and are not used when turnouts are renewed.
Undercut Switch	Switches for use with 50kg and 60kg rail have the stockrail undercut by machining to allow the switch to move partially under the head of the stockrail.
Asymmetric Switch	Switches used with tangential turnouts. They are not machined from rail. They have a thick web and are shallower than conventional and undercut switches.
Housed Switch	A heavy duty switch and joggled stockrail equipped with a "Housing". The housing is a specially machined component with a hardened checking face fitting above the switch to act as a checkrail for the opposite switch and joggle. Where both switches are required to be heavy duty a housing is required on one of the switches.
In - Bearer	A bearer fabricated into a hollow channel shape that is used at a set of points to house the switch operating rodding. This eliminates the rodding being located in a bay between bearers.
Interlocking	Interaction of equipment controlling switches and/or signals to prevent conflicting movements, and to make sure that routes are set correctly.

Term	Description
Chair Plates	A chair is a flat plate with a pressed up section that is attached with a bolt through the web of either stockrail, in the case of a switch assembly, or the checkrail carrier, in the case of a checkrail assembly.
Rail Brace	Component used in points assemblies to fasten the stockrail in position where fastenings on the gauge side of the rail cannot be used. The Rail Brace is bolted through the web of the stockrail.
Rail Brace Plates	Attach the Rail Brace to the bearer.
Switch Rollers	Rollers that support the switch during the opening and closing operation. They can be located in the bay between bearers, usually bolted to the stockrail, or be fabricated as a part of the plate assembly under the switch. They eliminate the need to lubricate the switch plate/switch interface.
Switch Stops	Switch Stops are bolted to the web of the stockrail and make contact with the web of the switch when the switch is in the closed position, providing lateral support. They can be manufactured from castings, rolled angle section or extended bolts.
Manual Point Lever	An apparatus consisting of a manually actuated lever and connecting rodding to operate points in turnouts and catchpoints or to operate a derail device. Manual point levers do not include ground frame or signal box levers that are generally connected to an interlocked signalling system.
Trailable Point Lever	A manual point lever that is designed to allow for vehicle wheels trailing through points set the wrong way to re-set the points for the trailing movement without the need to operate the lever.
Crossings	
Crossing Assembly	The component of a track system where lines branch out or intersect. Crossings assist in the passage of track wheels where two track rails intersect. Crossings may be fixed or switchable. In diamond crossings there are K and V crossings and in turnouts V crossings.
V crossing	A unit that allows a train travelling on the turnout direction rail to cross the mainline rail. The crossing rate is a measure of the angle made by the main line and turnout rail gauge faces that intersect at the theoretical point. The crossing rate is the cotangent of the angle made.
	All crossings are identified by markings on the wing rail which are provided during manufacture. See Appendix 2 Crossing Identification
	The catalogue number allows the geometry of the particular crossing to be identified. Each catalogue number defines a crossing with a unique geometry.
	See Appendix 2 for diagrams of standard crossing types
K Crossing	The principal special component of a diamond crossing. It is the intersecting component between two rails. The intersection creates an unchecked area in the centre of the K, thus limiting the angles that can be designed for K crossings
Fabricated Crossing	Comprises a V and two (2) wing rails fabricated from sections of rail, set, machined and fitted together with chocks. The hand of the crossing is determined by the location of the point rail and may be right or left. The point rail is always the rail carrying the maximum tonnages, or higher speed. A right hand crossing has the point rail in the rail that connects to the right hand switch.
Compound Crossing	Comprises a crossing V point that is manufactured from a single cast nose which is welded to head hardened rails to complete the V which replaces the point/housed rails in a fabricated crossing. They may be manufactured from manganese steel, chrome vanadium alloys or other materials.
Compound Manganese Crossing	A Compound crossing V point that is manufactured from a cast manganese nose which is explosively hardened and flashbutt welded to head hardened rails to complete the V. It replaces the point/housed rails in a fabricated crossing.
Fully cast crossing	A one piece solid cast steel crossing with the four legs joined to standard rail sections through a welding process or by bolts and plates.

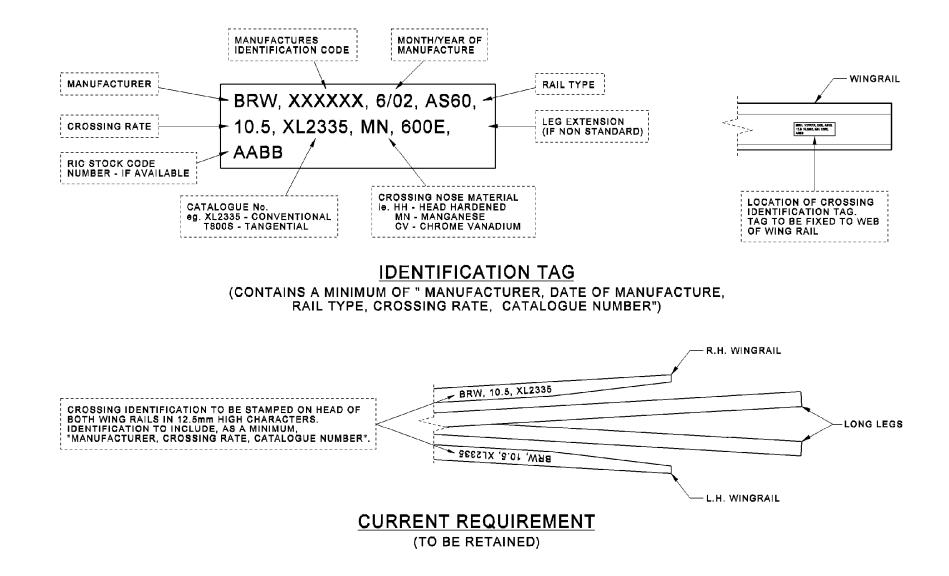
Term	Description	
Fixed crossings.	These crossings have a wheel flange gap in both rails. Wheel transfer at fixed crossings depends on matching wheel and rail profiles. Fixed crossings are used in conjunction with checkrails to provide lateral guidance in the crossing area.	
Switchable crossings.	These crossings close the gap in one track that is being made active for traffic allowing a continuous surface for the wheel to run through the crossing. Wheel transfer in switchable crossings is without any impact for any wheel profile. Switchable crossings have no flange gap in the active track and thus do not require checkrails. They can have either Swing Nose or Spring Wing	
Swing Nose Crossing	A switchable V crossing with a nose assembly that moves from the main line rail to the turnout rail, depending on the train movement, allowing a continuous surface for the wheel to run through the crossing. They are provided with straight crossings only. No checkrails are required with this crossing type.	
Spring Wing crossing	A switchable V crossing with both a fixed and spring wing leg. The spring wing effectively eliminates the flange way gap when using the main line thus reducing the wheel generated impact in the crossing. The wheel flange forces the spring wing open when taking the siding road.	
Wing Rail	The rails of a crossing (on the end closest to the switch in a turnout) that are flared to allow the passage of the wheel to transfer to or from the crossing nose. Named for their resemblance to a wing in shape.	
Flangeway	The space adjacent to the gauge face of a running rail to allow for the passage of wheel flanges.	
Flangeway Clearance	The distance between the gauge side of a running rail and the guard face of a checkrail or the guard face of a wing rail.	
Flangeway depth	Flange way depth is the height of the running surface of the rail above the top of the blocks at checkrails and in 'V' and 'K' crossings.	
Theoretical Point	Located on the crossing nose at the intersection of the gauge lines of the two running rails forming the crossing.	
Checkrail unit		
Checkrail Unit	The unit consists of a length of rail (called the checkrail) with a flared bevel machined on each end, hardened on the checking face, bolted through chocks to a closure rail (called the carrier) to attain a flangeway clearance. The centre of the checkrail is usually opposite the theoretical point of the crossing.	
Checkrail	A rail placed inside the running rail which comes into contact with the back of th wheel flange and is used in points and crossing work to provide steering of the wheelset such that the crossing nose is not contacted by the opposite wheel.	
Chocks	An iron casting used mainly with checkrails and crossings to support rail components at a fixed distance apart. Raised lettering and numbers on the chock identify its application.	
Flare	The tapered widening at the ends of flangeways to gradually engage wheel flanges and position them to pass through flangeways.	

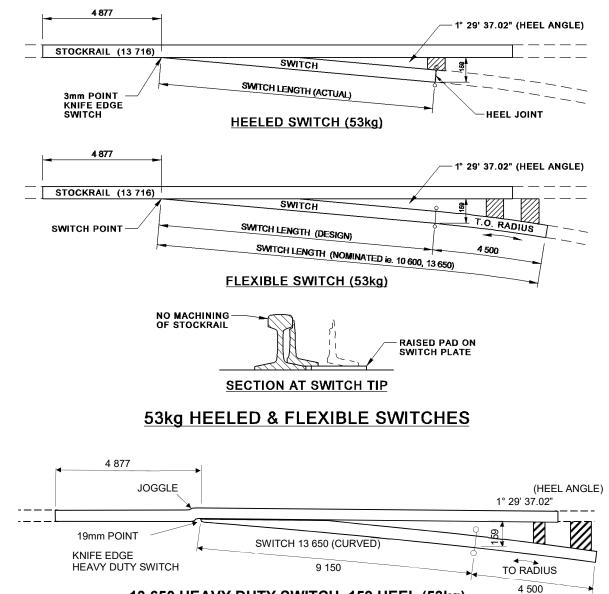
Appendix 2 General turnout data



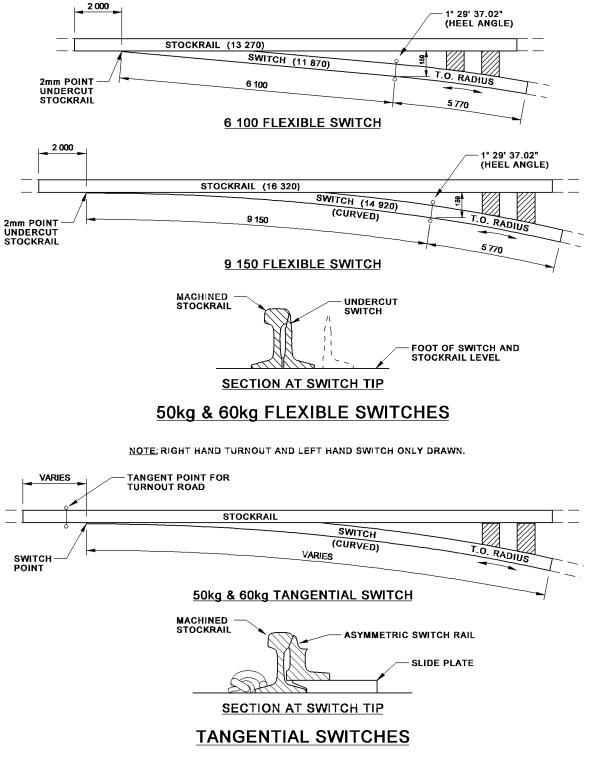




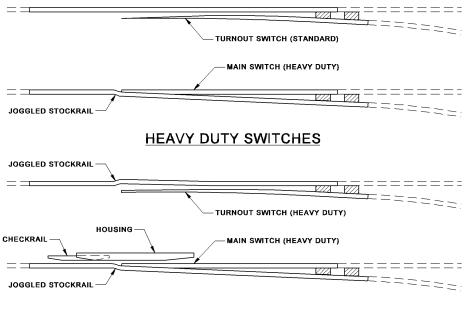




13 650 HEAVY DUTY SWITCH, 159 HEEL (53kg)



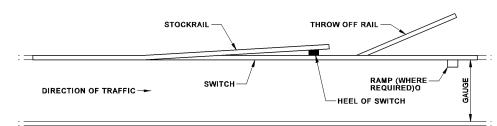
NOTE: RIGHT HAND TURNOUT AND LEFT HAND SWITCH ONLY DRAWN.



HOUSED SWITCHES

Appendix 3 Other special trackwork data

Catchpoints



CATCHPOINT CONFIGURATION

NOTE: SWITCH TYPE MAY BE HEELED OR FLEXIBLE

Appendix 4 Standard designs for conventional turnouts

	Standard Conventional Turnouts								
Rail		ossing	Quuitah	General Arrangement					
(kg)	Rate	Туре	Switch Description	Length	Bearers	Plating	Design Reference		
	0.05	Curved	5030 x 159 H	21.770	Timber	Resilient	720-420		
	8.25		6100 x 159 F	23.470	Timber	Standard	320-1197		
50	0	Straight	6100 x 159 F	23.510	Timber	Standard	320-1305		
50	9	Curved	6100 x 159 H	24.740	Timber	Standard	320-1520		
	10.5	Straight	6100 x 159 F	25.730	Timber	Standard	320-1309		
	10.5	Curved	6100 x 159 F	27.170	Timber	Standard	320-1310		
	0.05	Our and	5030 x 159 H	21.770	Timber	Resilient	246-466		
	8.25	Curved	10600 F	23.470	Timber	Resilient	246-403		
53	9	Straight	10600 F	23.510	Timber	Resilient	246-920		
	10.5	Straight	10600 F	25.730	Timber	Resilient	720-497		
	15	Straight	10600F / 13650F	32.270/35.320	Timber	Resilient	248-1180		
		Curved	6100 x 159 H	23.470	Timber	Resilient	320-1215		
	8.25		6100 x 159 F	23.470	Concrete	Resilient	690-418(RH) 690-419(LH)		
					Timber	Resilient	425-462		
	0	Straight	6100 x 159 F	23.510	Timber	Resilient	250-1258		
	9		9150 x 159 F	26.560	Timber	Resilient	250-1258		
					Timber	Resilient	720-615		
60	10.5	5 Straight Straight	Straight 6100 x 159 F 25.73	25.730	Concrete	Resilient	320-1282(RH), 720-436(LH)		
			9150 x 159 F	28.780	Timber	Resilient	720-615		
			6100 x 159 F	32.270	Timber	Resilient	425-725, 320-1219		
	15		9150 x 159 F	35.320	Timber	Resilient	425-725, 320-1219*		
			9150 x 159 F	35.320	Concrete	Resilient	720-538(RH), 720-539(LH)		

Table 13 - Standard Conventional Turnouts

- 1. H Heeled Switches.
- 2. F Flexible switches
- 3. For 53kg rail the flexible switch is defined as the total length of switch rail from which the switch is made. For 50kg and 60kg rail the flexible switch is defined as the length from the point to the theoretical head point (for design purposes only), and can be identified by the machining on the stockrail. (ie 53kg 10600 and 13650 switches have the same design geometry as the 6100x159 and 9150x159 (respectively) indicated for 50 and 60kg rail.
- 4. Standard Plating is a non-resilient type i.e. dogspikes, lockspikes, and/or screwspikes.
- 5. Resilient plating refers to an elastic type of fastener securing the rail foot to the baseplate

6. The layout for turnout bearers or ties forms part of the configuration. References to drawings detailing interface requirements for fixing components on standard turnouts, that is, crossings, checkrails, switch/stockrails and closure rails are indicated under design references.

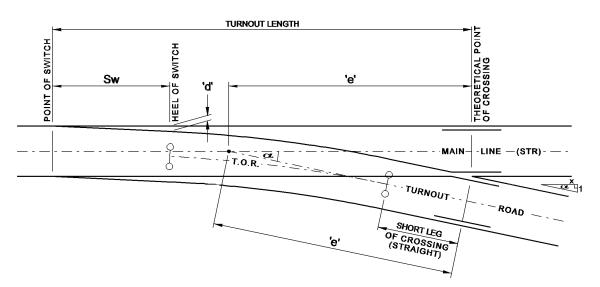


Figure 8 - Straight Crossing Conventional Turnout (drawn for RH turnout)

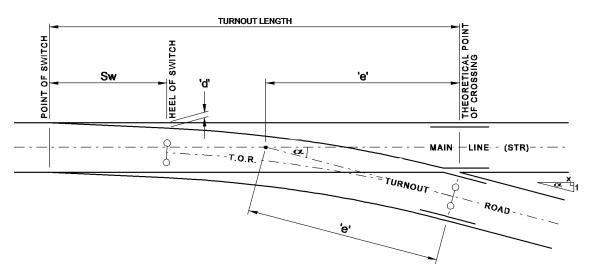


Figure 9 - Curved Crossing Conventional Turnout - short leg curved (drawn for RH turnout)

Sw

d

g

α

х

Crossing Rate	'e'
8.25	11.882
9	12.955
10.5	15.102
15	21.549

=	Switch length
=	Heel Centres (159mm)
=	Gauge (1435mm)
=	Crossing angle
=	Crossing rate

Switch length and heel centres are measured at heel joint for heeled switches and for flexible switches they are adopted for design purposes

Appendix 5 Standard designs for tangential turnouts

Tangential Turnouts – Design Parameters							
Туре	Crossing	Turnout Angle (º)	Length (T) (m)	Turnout Length (Pts to Theo Pt) (m)	Total Length (TOTP to TOEP) (m)	Distance (Pts to TP) (m)	General Layout Design Drawing Ref No.
160:6.6	Curved	8.615648	12.052	20.939	24.105	0.490	CV0479038
160:8.25	Straight	6.911227	9.622	21.058	24.644	0.490	CV0479039
190:7	Curved	8.130102	13.503	22.862	27.006	0.490	775-802
190:9	Straight	6.340192	10.523	22.988	26.298	0.490	775-801
250:8.25	Curved	6.911227	15.096	26.296	30.193	0.490	775-133
250:10.5	Straight	5.440332	11.878	26.489	30.309	0.490	775-134
300:9	Curved	6.340192	16.616	28.853	33.231	0.490	775-135
300:12	Straight	4.763642	12.478	29.238	33.630	0.490	775-136
500:12	Curved	4.763642	20.797	37.391	41.595	0.490	775-137
500:15	Straight	3.814075	16.648	37.707	43.532	0.490	775-003
800:15	Curved	3.814075	26.637	46.827	53.274	1.090	775-138
800:18.5	Straight	3.094058	21.606	47.083	54.660	1.090	775-139
1200:18.5	Curved	3.094058	32.409	56.996	64.818	1.690	775-140
1200:24	Straight	2.385944	24.989	57.754	67.026	1.690	775-141

Table 14 - Standard Tangential Turnouts

Tangential Turnouts – In-bearer design						
Туре	Comment	General Layout Design Drawing Ref No.				
190	no back-drive required	CV0278550				
250	with backdrive	CV0278551				
300	with backdrive	CV0278552				
500	with backdrive	CV0278553				

Table 15 – Standard In bearer layouts for tangential turnouts

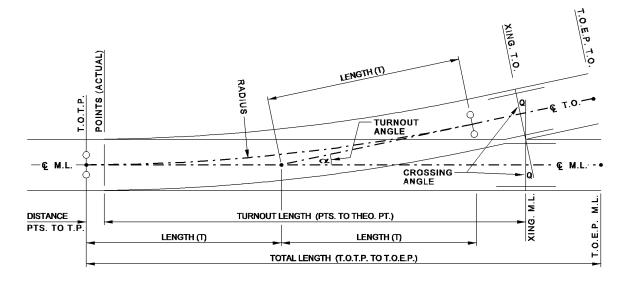


Figure 10 - Straight Crossing Turnout (drawn for LH turnout)

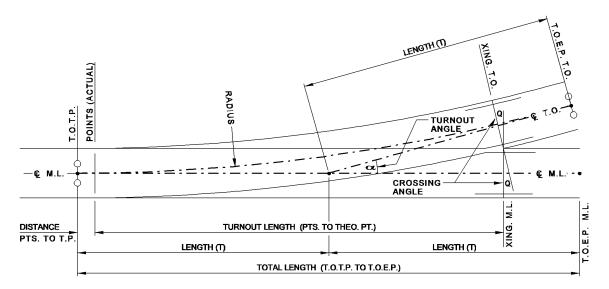


Figure 11 - Curved Crossing Turnout (drawn for LH turnout)

Appendix 6 Approved products

The approved product list for turnouts and special trackwork contains only those products that may be used independently of any manufacturer's proprietary designs.

Product approvals are dependent on both the manufacturer and supplier. If either changes, the product approval may no longer be valid. Seek advice from the Principal Track and Civil Engineer.

Product Approval Numbers are shown for all products approved by JHR CRN. Other products listed were approved for use on CRN prior to January 2012 and have been accepted by JHR CRN.

Product Approval No.	Common Item Name	Description	Standard/ Drawing	Manufacturer/ Supplier
Manual lev	ers			
	Thornley levers	Туре 45		VCAU
Switch equ	ipment			
	Switch roller plates			
	Switch pad protectors	Mack Reversible Switch Protector		VCAU
	Chair Bolt Cat. No 3	M24 x 75 Square Head Chair Bolt Cat. No3	Dwg. No 91-187C	Greg Sewell Forgings
Crossings				
	Compound manganese	Fully cast manganese crossings (Monobloc)	CRN CS 250	VAE
	Rail Bound Manganese			VCAU

Appendix 7 Approved special configurations

The following configurations are approved variations from standard configurations. They are applicable to the nominated locations only. When due for replacement they shall be replaced by standard configurations.

Configuration Type	Approved variation	Location		Controls	Original Waiver
Catchpoints	Shorter switch Victorian design catchpoints	AWB sidings West Wyalong and Stockinbingal	r a c r	All other aspects of CRN catchpoint standards to be met including, landing area, throw off rails, derailment block, clearance requirements Maximum speed 15kph	CCW 12/002 10/1/2012
Turnout	Allow heeled switches and mechanical joints in main line	Ardlethan 555.748	- - - - - - - - - -	Replace turnout with fully complying turnout. If CWR in section is to occur before installation of new turnout leave one adjustment length on all sides (with temporary creep pegs) and adjust to CWR after turnout installation. The adjustment length on all sides is to comply to and be managed as LWR in the interim.	CCW 15/018 14/07/2015

Appendix 8 Crossing nose profiles

The design profiles are defined by the nose depths at the 16mm point and the 32mm point. A straight is formed by these two locations shown as A and B in Figure 12.

Select the profile to be used on any particular crossing by referring to Table 17. Select the profile based on the flangeway width at the crossing, wingrail profile, traffic task and whether the crossing is facing, trailing or both.

Longitudinal Profile				
Nos	e Width	32mm		
Nose Depth		Α		
Facing Profiles	F1	A= 1mm]	
	F2	A= 2mm		
	F3	A= 3mm		
Trailing Profiles	T1	A= 1mm		
	T2	A= 2mm		
	Т3	A= 3mm]	

Table 16- Longitudinal Profiles

Figure 12 – Crossing nose design slope

Profile Selection					
Traffic direction Facing or Both					
Wing	44 Flangeway	42 Flangeway			
Standard wing rail rounded shape	F1	F2			
Square Wing	F2	F3			
Traffic direction	Trailing Only				
Wing	44 Flangeway	42 Flangeway			
Standard wing rail rounded shape	T1	T2			
Square Wing	T2	Т3			

Table 17- Longitudinal Crossing Profile Selection

Square wingrails (see Figure 13) provide greater support for the wheel and allow a longer nose ramp. VAE achieve a square wingrail by machining a standard rail. Monoblock and RBM crossings are designed with a square wing.

Figure 13 - Cross-Section showing square vs rounded wing

Appendix 9 – Determination of speed of runaway train in siding or loop

To determine the speed that a train will roll can be approximated using a number of factors, which can by generalised as:

- Change in height over which the runaway rolling stock may pass
- Rolling resistance of the rolling stock
- Length of the siding/loop
- Initial speed

Due to complexities in determining and in doing so, only makes estimates more conservative, it is permissible to ignore to effects of:

- Wind
- Curves
- Friction

Using the conservation of energy the final speed of the vehicle can be estimated as

$$v = 3.6 \sqrt{\left(\frac{u}{3.6}\right)^2 - 2g\left(h + \frac{fs}{1000}\right)}$$

Where

v = final speed of the train (km/h)

- u = initial speed of the train (km/h)
- g = acceleration due to gravity (9.81m/s²)

h = change in elevation (m, where negative values indicate a decrease in elevation)

f = rolling resistance of the vehicle (to be taken as 1.5kg/tonne of vehicle mass)

s = distance travelled